



Various battery models for various simulation studies and applications



S.M. Mousavi G.^{*}, M. Nikdel

Centre of excellence for Railway school, The School of Railway Engineering, Iran University of Science and Technology, Tehran, Iran

ARTICLE INFO

Article history:

Received 12 March 2013

Received in revised form

7 January 2014

Accepted 13 January 2014

Available online 1 February 2014

Keywords:

Battery model

Mathematical model

Electrical based-model

Electrochemical-based model

ABSTRACT

Batteries are one of the most common devices used for saving electrical energy in various applications. It is necessary to understand the battery behavior and performance during charge and discharge cycles. An accurate model of a battery with a specific application is needed for an appropriate analysis and simulation. Therefore, in the field of battery modeling, various models have been proposed. This paper presents an overview of several electrical battery models. These models are classified into six categories. The parameter details of a battery model will not be computed but a brief description of them is given. Furthermore, the applications of each model are discussed. Finally, a comparison between presented models will be made.

© 2014 Elsevier Ltd. All rights reserved.

Contents

1. Introduction	477
2. Simple battery models	478
2.1. Ideal battery model	478
2.2. Simple battery model	478
2.3. Modified simple battery model 1	478
2.4. Modified simple battery model 2	479
2.5. Modified simple battery model 3	479
2.6. Modified simple battery model 4	479
3. Thevenin-based battery models	480
3.1. Thevenin battery model	480
3.2. Modified Thevenin battery model 1	480
3.3. Modified Thevenin battery model 2	480
3.4. Modified Thevenin battery model 3	480
3.5. Modified Thevenin battery model 4	481
3.6. Modified Thevenin battery model 5	481
3.7. Modified Thevenin battery model 6	481
4. Impedance-based battery models	481
5. Runtime-based battery model	482
6. Combined electrical circuit-based model	482
7. Generic-based model	483
7.1. Generic battery model	483
7.2. Modified generic battery model	483
8. Conclusion	484
References	485

1. Introduction

Nowadays, energy storages have numerous applications. Batteries are the most famous of them. They are applied in several

^{*} Corresponding author.

E-mail address: sm_mousavi@iust.ac.ir (S.M. Mousavi G.).

industries such as in electrical and hybrid vehicles [1–7], renewable energy systems [8–12], and marine current energy systems [13]. Batteries serve as a backup in wind energy conversion systems (WECS) or photovoltaic (PV) systems. They are implemented to store excess energy captured from wind energy or sunlight using wind turbines during windy or sunny days and also for releasing the stored energy during stationary times or at night time [8,9]. Another application of battery storage is in aerospace satellites. They are used to collect energy using PV panel for satisfying required energy when the satellite is exposed to the sun and to release the energy during eclipse [14]. In electric or hybrid trains and vehicles, a battery is used for storing energy from regenerative braking system and returning the energy to the system when the train is in traction mode [1–7]. Batteries can play a significant role when they used with other storages such as fuel cells, ultra-capacitors, and super-magnetic energy storages (SMES). They can increase reliability of the hybrid systems [15,16]. Various flexible AC transmission system (FACTS) devices such as dynamic voltage resistor (DVR), and static compensator (STATCOM) utilize a battery for improving power quality of electrical voltage such as voltage sags [17]. Furthermore, the battery accompanied by an inverter is implemented in an uninterruptible power supply (UPS) in order to satisfy the loads and burdens during voltage sag and power interruption [18]. In all the above mentioned applications, an accurate modeling and simulation of a battery for examining system performance is necessary. Battery modeling involves two categories of electrochemical modeling and electrical circuit modeling. The electrochemical model of a battery is structurally based on the internal electrochemical actions and reactions of a cell. It is not obtained from an electrical network. Although accurate, this model is complex and needs a precise recognition of the electrochemical processes in the cell. It is not applied in power and dynamic systems studies. Electrical circuit modeling is another useful model presented by many researchers. In the electrical circuit modeling, the electrical characteristics of the battery are considered and passive linear elements are used. Such models are easy to understand. For example, the battery capacity is modeled by a capacitor. Given that the voltage and internal resistance of a battery are dependent on temperature and state of charge, open circuit voltage of a battery represented by a controlled dc voltage source is changed by the state of charge and temperature. Moreover, internal resistance is modeled by variable resistance. The value of the internal resistance is changed by the state of charge and temperature as well. In this paper, the electrical circuit models are classified into six overall models. These models consist of simple models, Thevenin-based models, impedance-based models, runtime-based models, combined electrical circuit-based models, and generic-based models. Specifications and applications of each model are considered and discussed. Finally, advantages and disadvantages of each model are presented below.

2. Simple battery models

In this section, six simple-based models of a battery will be described briefly as follows.

2.1. Ideal battery model

The ideal battery model is the simplest model because the internal parameters are neglected. It is represented by only an ideal voltage source. This model is shown in Fig. 1 [19]. It is mainly suitable in some simulations where the energy released from the battery is supposed to be infinite. In this model, the state of charge and internal parameters of the battery are not considered.

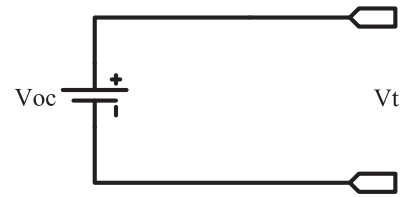


Fig. 1. Ideal battery model.

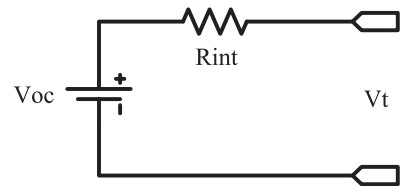


Fig. 2. Simple battery model.

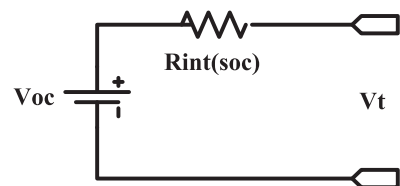


Fig. 3. Modified simple battery model 1.

Furthermore, the application of this model is mainly in the simulation of slag bus in steady state studies of power systems.

2.2. Simple battery model

A simple battery model, shown in Fig. 2, is composed of a series of internal resistance connected to an ideal voltage source. State of charge (SOC) is not considered in this model. In this figure, V_o is an ideal open-circuit voltage, V_t is the terminal voltage of battery and R_{int} is the internal series resistance. In the simple battery model, V_t can be clarified by an open circuit voltage measurement test. R_{int} is assumed to be constant while it is changed when a load is connected to a battery. Thus, this model is just appropriate in circuit simulations where the energy released from the battery is supposed to be infinite or the state of charge is not important [20]. For example, this model is not suitable for electric trains or vehicles application. However, it can be used with ultra-capacitor or fuel cell as hybrid energy storage. Also, this model is applied as an input source connected to the inverter power electronic devices [21].

2.3. Modified simple battery model 1

A model made up of an ideal voltage source accompanied by an internal resistance is discussed in [22]. Here, the voltage source and internal resistance are a function of the SOC. This model is shown in Fig. 3. In this battery model, the state of charge is considered by making the R_{int} and V_{oc} of battery changes in accordance with its state of charge. R_{int} is determined through following equation:

$$R_{int} = \frac{R_0}{S^K} \quad (1)$$

where S and R_0 are the state of charge and initial battery internal resistance respectively. R_0 is calculated when the battery is fully

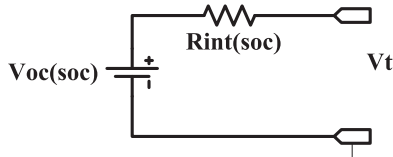


Fig. 4. Modified simple battery model 2.

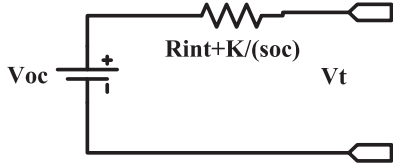


Fig. 5. Modified simple battery model 3.

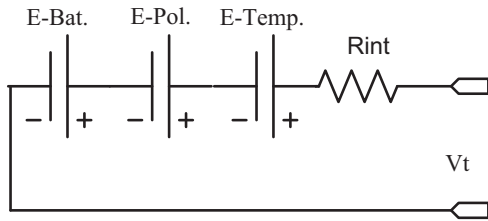


Fig. 6. Modified simple battery model 4.

charged:

$$S = 1 - \frac{Ah}{C_{10}} \quad (2)$$

In the above equation, C_{10} is ten-hour capacity (Ampere–hours) at the reference temperature. A and h are the current and time of discharging process respectively. S changes from 0 (when battery is discharged) to 1 (when battery is fully charged). K is a constant designated capacity coefficient. It is related to discharge rate. It is computed based on k_1 , k_2 and k_3 . The coefficients of k_1 , k_2 and k_3 are constants specified using the curves supplied by the manufacturers. They are related to three different charge rates. Furthermore, the capacity of the battery changes using the coefficient of K under different discharge rates. This model has been applied by many battery manufacturers for battery monitoring aims. This model does not explain for the capacitance effect as an example of the transient current conditions taking place in the battery. It is used for modeling of a sealed lead acid battery applied in an uninterruptible power supply [23].

2.4. Modified simple battery model 2

In this model, shown in Fig. 4, the battery is used as a voltage source connected to a series resistance. The voltage and internal resistance are related to the state of charge (SOC). The open circuit voltage is described as

$$V_t = V_{oc}(SOC) - IR_{int}(SOC) \quad (3)$$

where $V_{oc} = f(SOC)$ is the no load voltage of the battery and $R_{int} = f(SOC)$ is the internal resistances of discharge and charge cycles, where

$$V_{oc} = V_o - A \cdot D \quad (4)$$

$$R_{int} = R_o - B \cdot D \quad (5)$$

where V_o is open circuit voltage (battery is in full charge), D is the state of discharge, R_{int} is the internal resistance (battery is in full

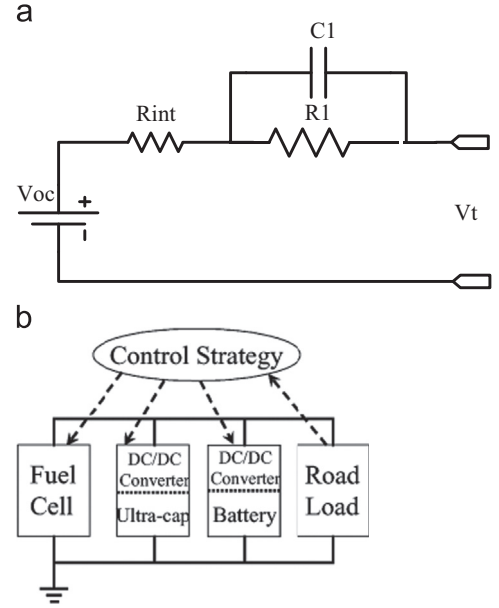


Fig. 7. (a) Thevenin battery model. (b) Hybrid of battery and fuel cell and ultra capacitor.

charge), and A , B are constants obtained from experiments. This model does not account for the transient condition [24]. This model is applied in a single phase inverter system in order to generate an alternative voltage from a DC voltage for satisfying an AC load such as an induction motor.

2.5. Modified simple battery model 3

The modified simple battery model 3, shown in Fig. 5, is developed based on the Thevenin battery model. The open circuit voltage and internal resistance are nonlinear characteristics indicated by K/SOC [25]:

$$V_t = V_{oc} - \left(R_{int} + \frac{K}{SOC} \right) I \quad (6)$$

where V_t is terminal voltage of battery, V_{oc} is no load circuit voltage, R_{int} is battery terminal resistance, K is polarization constant, and I is discharge current. This model is implemented in the modeling of lead acid battery used in traction systems [25].

2.6. Modified simple battery model 4

This model, shown in Fig. 6, is structurally based on three voltage sources and an internal resistance. Each element modeled in PSPICE software is described as follows:

- (1) E-bat. (E-Battery): This is an ideal voltage source that displays the voltage in the cells.
- (2) E-pol. (E-polarization): It shows the effects of polarization caused by the active materials availability in the battery.
- (3) E-Temp. (E-Temperature): It displays the temperature effect on the terminal voltage of the battery.
- (4) Rint. (Internal Resistance): This is the internal impedance of the battery.

The value of each element is dependent on the relationship between voltage and the state of charge of the battery cell. This model is relatively accurate and can be used for Ni–Cd and Li-ion batteries and applied in the charge and discharge cycles. Also, it could be applied to traction applications or electric/hybrid vehicles [26].

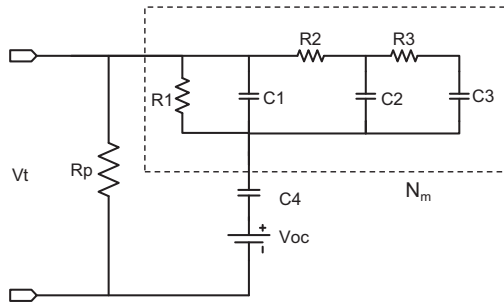


Fig. 8. Modified Thevenin battery model 1.

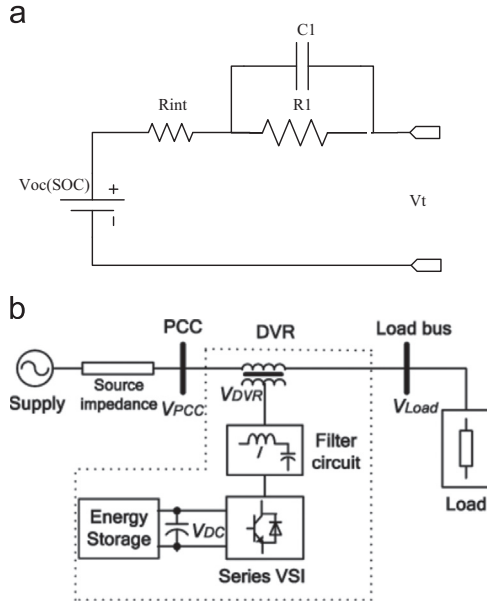


Fig. 9. (a) Thevenin battery model 2. (b) Battery storage applied in a dynamic voltage resistor.

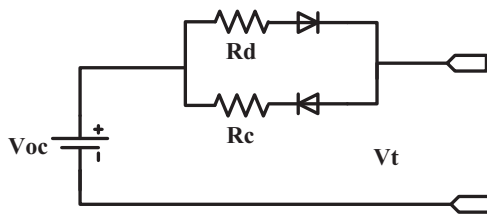


Fig. 10. Modified Thevenin battery model 3.

3. Thevenin-based battery models

In this section, seven Thevenin-based models of a battery will be described briefly as follows.

3.1. Thevenin battery model

Transient behavior of the battery has not been investigated in the previous models. Thevenin battery model is composed of an ideal voltage source (V_{oc}), an internal resistance (R_{int}), an over-voltage resistance (R_1) and a capacitor (C_1). The configuration of this model is shown in Fig. 7a. C_1 and R_1 show the capacity of parallel plate and the resistance implicated by the contact resistance of the plate respectively. The major shortcoming of the Thevenin battery model is that all the parameter values are assumed to be constant, while all the parameter values are related to the SOC, storage capacity of the battery, discharge rate,

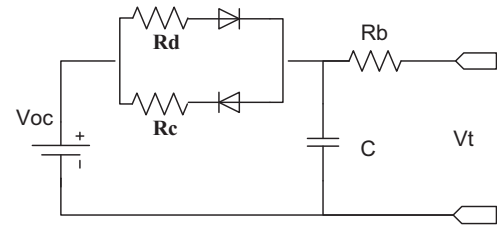


Fig. 11. Modified Thevenin battery model 4.

temperature and some other characteristics of discharge. The application of this model is in hybrid power train modeling where the battery is combined with fuel cell/ultra capacitor energy storage shown in Fig. 7b [27,28].

3.2. Modified Thevenin battery model 1

Thevenin model has been improved using a linear electrical battery model shown in Fig. 8 [29]. This model is better than previous ones because the behavior of the battery during over-voltage and self-discharge of the battery is considered. Although it is more accurate than previous models, the changes of the parameter values according to different operating conditions in previous models have been ignored. In this model, R_p is self-discharge resistance, and C_4 is electrochemical capacitance of the battery cell. N_m which is the battery cell overvoltage network consists of resistances of R_1, R_2, R_3 and capacitors of C_1, C_2 , and C_3 . These parameters are given based on the measured electrical response of the battery. Furthermore, V_{oc} is the open circuit voltage of the battery. This model is utilized for transient and steady state analysis of electrical systems working with batteries.

3.3. Modified Thevenin battery model 2

This model takes the transient behavior of a battery consists of an RC parallel network (R_1 and C_1 are overvoltage resistance and double layer capacitance respectively) for the transient behavior of a cell, and an ohmic resistance R_{int} for the instantaneous voltage drop shown in Fig. 9a. The battery runtime cannot predict in this model as well. The DC response of the battery cell cannot be modeled. The open circuit voltage, V_{oc} , relates to the SOC [30]. Voltage sag is defined as a short reduction in effective voltage of a bus-bar. It is often created through short circuit, overloading, and starting of large electrical motors. Dynamic voltage resistor (DVR), shown in Fig. 9b, is a FACTS device applied to remedy the sag of the voltage. It consists of a battery and pulse width modulation (PWM) inverter. This model is applied in the DVR system [17] as well as in photovoltaic systems [31].

3.4. Modified Thevenin battery model 3

This modified simple battery model (shown in Fig. 10) is a compound of an ideal voltage source connected to two series of internal resistance. They consist of discharging and charging resistances. As this figure shows, R_d and R_c are the internal resistances of the discharging and charging mode respectively. Both these resistances consume energy. Therefore, they express energy losses containing both electrical and non-electrical losses. The diodes in the model are supposed to be ideal. They are applied to bypass internal resistances during charging or discharging cycles. Both charging and discharging cycles do not conduct simultaneously. The conducting diode is forwardly biased and the other diode is reversely biased. It is supposed that the diodes have no interpretation. They are just to clarify the difference between the charge and discharge resistance. Dependency on

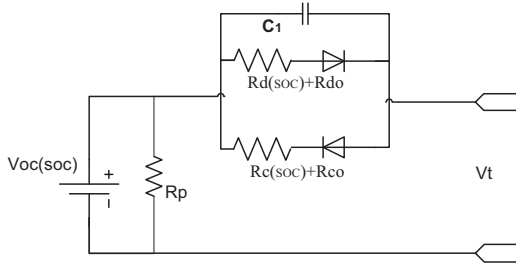


Fig. 12. Modified Thevenin battery model 5.

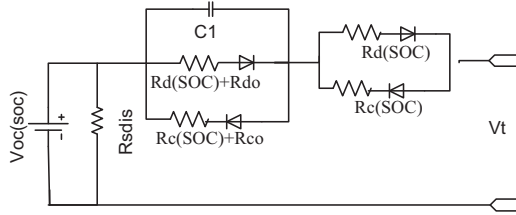


Fig. 13. Modified Thevenin battery model 6.

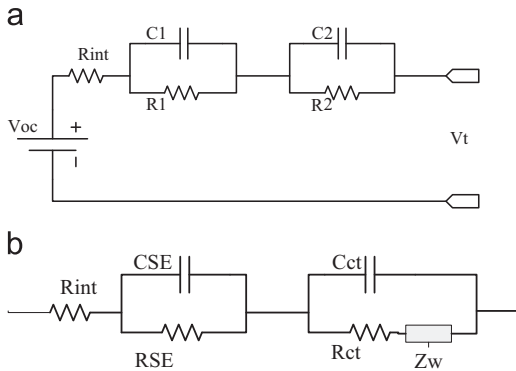


Fig. 14. (a) Impedance battery model. (b) The battery equivalent internal impedance.

the SOC is not considered in this model, hence the main disadvantage of this model. All the elements in this model are linear, and this is yet another disadvantage. This model is implemented in electric/hybrid vehicles simulations [32].

3.5. Modified Thevenin battery model 4

This battery model, alias reactive circuit model, is similar to the model described in modified Thevenin battery model 3 and presented in [32]. The dynamic electrical equations of the circuit model for charging and discharging cycles are obtained as follows:

$$\frac{dV_p}{dt} = -V_p \frac{1}{R_d C} + V_{oc} \frac{1}{R_d C} - I_b \frac{1}{C}, \quad V_p \leq V_{oc} \quad (7)$$

$$\frac{dV_p}{dt} = -V_p \frac{1}{R_c C} + V_{oc} \frac{1}{R_c C} - I_b \frac{1}{C}, \quad V_p > V_{oc} \quad (8)$$

where

$$I_b = \frac{V_p - V_{oc}}{R_b}$$

V_{oc} is the open circuit voltage; V_p is capacitor voltage and V_t is the terminal voltage of the battery. R_c , R_d and R_b are the charging, discharging and the internal resistance of the battery respectively; C is the polarization capacitance of the battery and I_b is current of

the battery. In this circuit model portrayed in Fig. 11, the SOC of the battery can be easily computed under open circuit voltage i.e. when $R_b = 0$, $V_t = V_p$. Both of them converge exponentially toward V_o with a time constant concluded by R_d . This model is applied in electric or hybrid vehicles simulations.

3.6. Modified Thevenin battery model 5

All the elements of this model relate to the state of charge shown in Fig. 12. The elements' characteristics are described below

Self-discharge resistance (R_p): This resistance is a function of the open circuit voltage. It concerns for resistances in:

- Electrolysis of water in the battery at high voltage.
- Slow leakage of the battery terminal at low voltage.

Charge and discharge resistances (R_c and R_d): These relate to electrolyte resistances, plates and fluid resistance; however, all these resistances can be different in charging and discharging cycle and rate.

Overcharge and over discharge resistance (R_{co} and R_{do}): These are the internal resistances that will be changed when the battery is overcharged or over discharged. There is a capacitor in the model which explains the battery transient behavior [33]. This model is applied in electric or hybrid vehicles simulations too.

3.7. Modified Thevenin battery model 6

This model, shown in Fig. 13, is an improvement of the previous battery models i.e. modified Thevenin battery model 5. It contains nonlinear characteristics. It is dependent on the state of charge. The elements of this model are the functions of the state of charge or the open circuit voltage which dependent on the state of charge. This model consists of a series of experimental tests performed through examination of the graphic plots of the experimental data, and manufacturers' specifications. Two ideal diodes have been implemented to recognize between overvoltage resistance and internal resistance for charge and discharge cycles [30]. Because this model is a developed version of the previous one, it has been implemented in electric or hybrid vehicles and trains simulations [33,44].

4. Impedance-based battery models

Impedance-based model is another electrical model shown in Fig. 14a. The impedance elements in this model are clarified using electrochemical impedance spectroscopy (EIS) measurements to achieve the AC response of a cell at certain frequency spans. The results are depicted on a chart named Nyquist diagram. This chart consists of a real axis representing the resistance of the cell and the imaginary axis representing the reactance of the cell. Each point in this area is stated with the impedance response at a specific frequency. This is mostly performed using implementation of a small-amplitude sinusoidal current or voltage signals to the system and checking the response for different frequencies. The reason for using this method is to keep the system in the linear region. Then, the response will have the sinusoidal shape and so likely with different amplitudes and phase angles. The internal impedance of the battery which is dependent on the electrochemical processes in the cell is modeled in Fig. 14b known as Randle circuit. In this model, R_{int} is the bulk resistance, describing the electric conductivity of the electrodes and the separator. R_{SE} and C_{SE} are the symbols of resistance and capacitance of the surface film layer on the electrodes. R_{ct} is the charge transfer resistance. It relates to the charge transfer between electrode and the

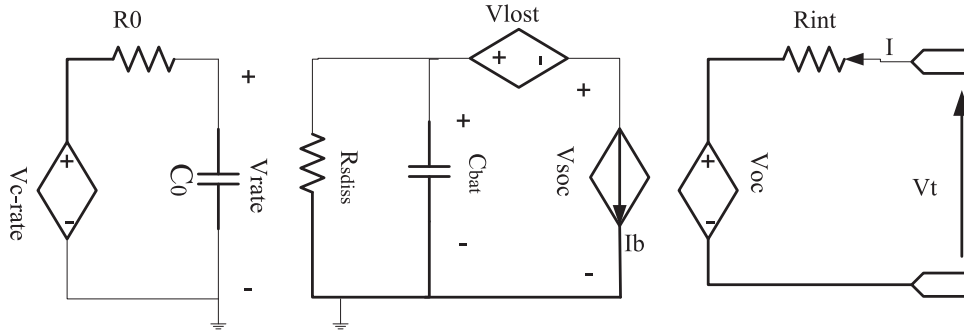


Fig. 15. Runtime-based model.

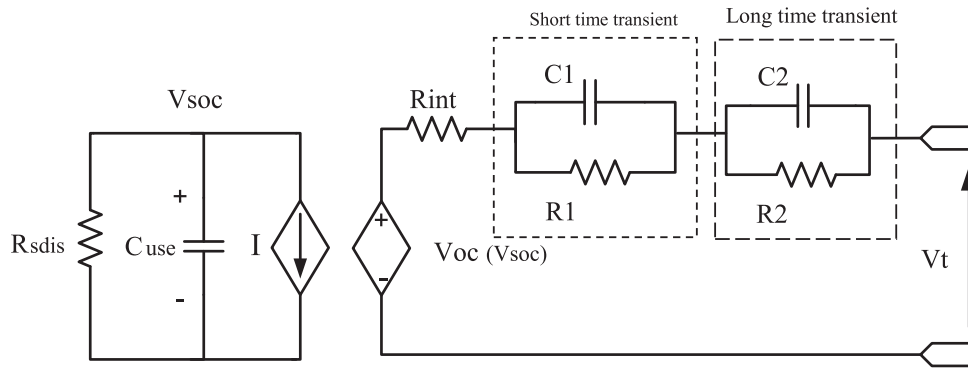


Fig. 16. Combined electrical circuit-based model.

electrolyte. C_{dt} is double layer capacitance between the electrode and electrolyte. R_{ct} and C_{dt} demonstrate the medium frequency response. Z_W is designated as the Warburg impedance. In the lithium ions battery, the diffusion of the lithium ions between the electrolyte and active material is presented using this impedance at the low frequency response. RC pair is implemented to increase the accuracy of the model. Thus, it can be replaced with a resistance when accuracy is not very important. Furthermore, in some cases an inductance is joined to a series bulk resistance for explaining the positive reactance response at high frequencies. Likewise, the positive reactance response can be neglected [34–38]. This model can be applied to traction electric/hybrid vehicles modeling and simulation.

5. Runtime-based battery model

The equivalent circuit of battery cell, shown in Fig. 15, is called runtime-based circuit model. It is a complex model for simulation of runtime and DC response under a constant discharge current. It can be modeled for a limited transient response [39]. In this model, the following effects are considered: (1) the voltage of the battery is dependent on the SOC. When the battery is discharged, V_t diminishes by a varied rate; (2) the battery's actual capacity is dependent on discharge rate. Conversion of chemical energy into electrical one diminishes by increasing rate; (3) total charge quantity is affected by discharge current frequency. This model consists of three separated circuits. The left circuit indicates the dependency on discharge frequency. It consists of R_0 , C_0 , and V_{c-rate} . R_0 and C_0 are transient elements. They are referred to as charge storage resistor and charge storage capacitor respectively. They created a low pass filter in order to control V_{lost} . The middle circuit indicates the dependency on the state of charge and discharge rate. It consists of V_{lost} , C_{bat} , R_{sdiss} and current source of

I_b . V_{lost} indicates the dependency on discharge rate. It diminishes the charge of the battery and controls the output voltage. The magnitude of V_{lost} is a function of the discharge rate. It is modeled using a look up table. C_{bat} and R_{sdiss} are battery capacitor and self-discharge resistor respectively. Finally, the right circuit consists of an open circuit voltage (V_{oc}), and internal resistor of the battery (R_{int}). This model has been applied to traction electric/hybrid vehicles modeling.

6. Combined electrical circuit-based model

This model, shown in Fig. 16, is a combination of the Thevenin, impedance and runtime-based electrical circuit models. It consists of two separate parts: energy balance and voltage response circuits. The first part models the capacity of the cell, the amount of energy remaining in the battery cells, the self-discharge, and the battery runtime. The capacity of the battery is indicated by C_{use} . The C_{use} is not an actual capacitance. The voltage of V_{soc} changes between 0 and 1, tantamount to the battery state of charge. Thus, the SOC will be utilized instead of V_{soc} . It changes (increases or decreases) depending on the charge or discharge current respectively. Self-discharge of the battery is modeled by a resistor shown by R_{sdiss} . The second part (voltage response) explains how battery voltage changes to a given load current (I). Open circuit voltage is a dependent supply voltage which depends on the state of charge, presented by V_{soc} . R_{int} is the Ohmic resistance of the battery. It consists of the bulk resistance R_b and surface layer resistance R_{SEI} . R_1 and C_1 are the symbols of the short time constants in the voltage response. They are dependent on the charge transfer resistance (R_{ct}) and double layer capacitance (C_{dl}). The long time constants are shown by R_2 and C_2 , connected to a single RC pair Warburg impedance in order to model diffusion phenomena

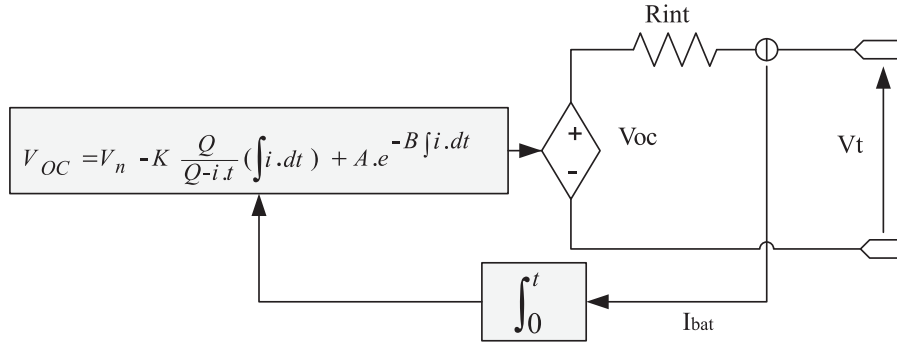


Fig. 17. Generic battery model.

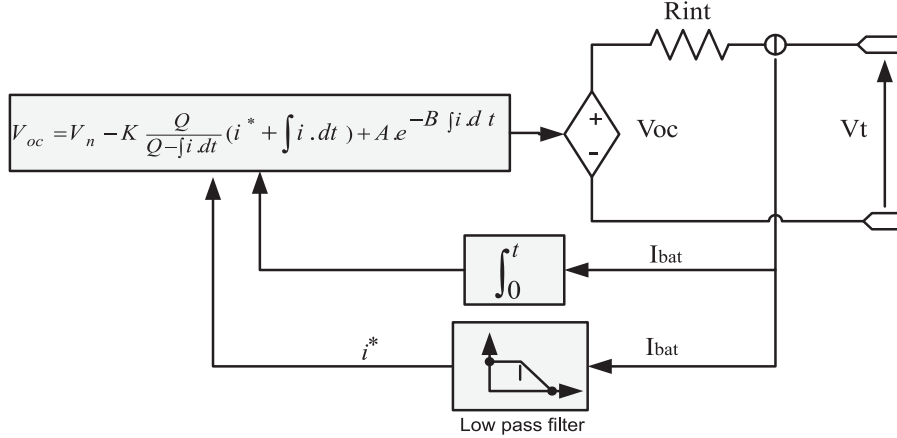


Fig. 18. Modified generic battery model.

[39,40]. This model can be implemented in simulating a traction system or in electric/hybrid vehicle modeling.

7. Generic-based model

7.1. Generic battery model

A generic battery model consisting of a controlled voltage source connected to a resistance can be applied for modeling of various types of electrochemical batteries. This model is shown in Fig. 17. The model's parameters can be obtained from the manufacturer's discharge curve. This model is easy to use. It can be implemented to simulate a type of battery using dynamic simulation software such as Matlab/Simulink. In this model, state of charge of the battery can be implemented as a state variable for avoidance of the mandatory loop problem [41].

Based on Fig. 17, the equation is obtained from shepherd equation. The shepherd equation model is given as follows:

$$V_{oc} = E_0 - K \frac{Q}{Q - \int i \cdot dt} i - R_0 i \quad (9)$$

where E_0 is open circuit voltage of the battery, Q is capacity of the battery, K is polarization resistance coefficient, R_0 is internal resistance, and i is battery current. There is a nonlinear term in the shepherd equation i.e. $Q/(Q - \int i \cdot dt)$.

This term states how the voltage is varied by real charge and current of the battery. In order to eliminate the algebraic loop, the shepherd equation is modified as in the following equation:

$$V_{bat} = E_0 - K \frac{Q}{Q - \int i \cdot dt} i + A \cdot \exp(-B \cdot \int i \cdot dt) \quad (10)$$

In this model, the following suppositions are implemented:

The internal resistance of the battery does not change during the charge and discharge. Pukert effect and temperature on battery capacity are not included. The memory effect and self-discharge of the battery are ignored.

7.2. Modified generic battery model

A modified generic battery model is shown in Fig. 18. It is a modified model of the previous one. It presents the charge and discharge cycle of the battery using the following equations based on the Shepherd equation [42]:

$$V_{dis} = E_0 - K_{dr} \frac{Q}{Q - \int i^* \cdot dt} i^* - R_0 i - K_{dv} \frac{Q}{Q - \int i^* \cdot dt} i + \exp(t) \quad (11)$$

$$V_{ch} = E_0 - K_{cr} \frac{Q}{\int i^* \cdot dt + \lambda Q} i^* - R_0 i - K_{cv} \frac{Q}{Q - \int i^* \cdot dt} i + \exp(t) \quad (12)$$

where Q is battery capacity, k_{dr} and k_{cr} are the polarization resistance coefficient at discharge and charge cycles respectively. k_{dv} and k_{cv} are the polarization over voltage coefficient at discharge and charge cycles respectively. In the second term of Eqs. (11) and (12), the polarization Ohmic voltage drops are different for charge and discharge cycles. They are modified using filtered battery current (i^*) to simulate the dynamic response of the real slow voltage at step current response. The λ in Eq. (12) is used to shift the polarization resistance during the charge cycle of the battery. The third term in the above equations refers to internal resistance for charge and discharge cycles. The fourth term of the equation is added to this term with respect to the polarization overvoltage. This term, accompanied by E_0 , can better describe the nonlinear open circuit voltage relationship with the state of charge. The $\exp(t)$ term explains an exponential dynamic voltage to bring a nonlinear hysteresis

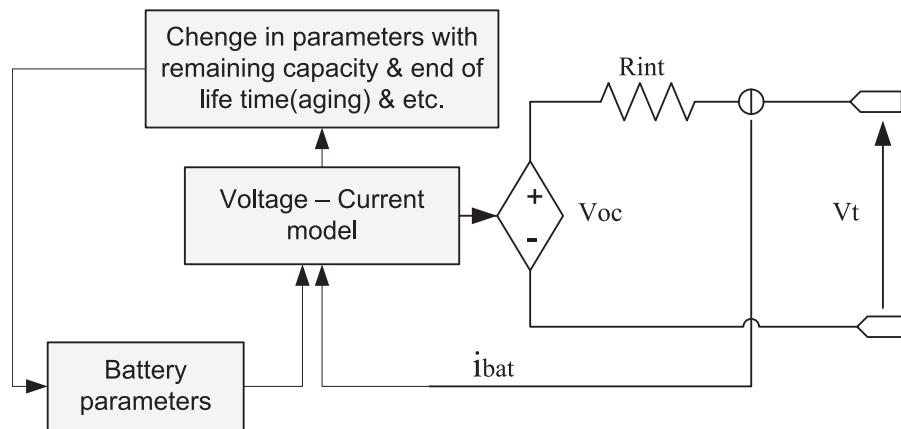


Fig. 19. Generic battery model with changes in parameters.

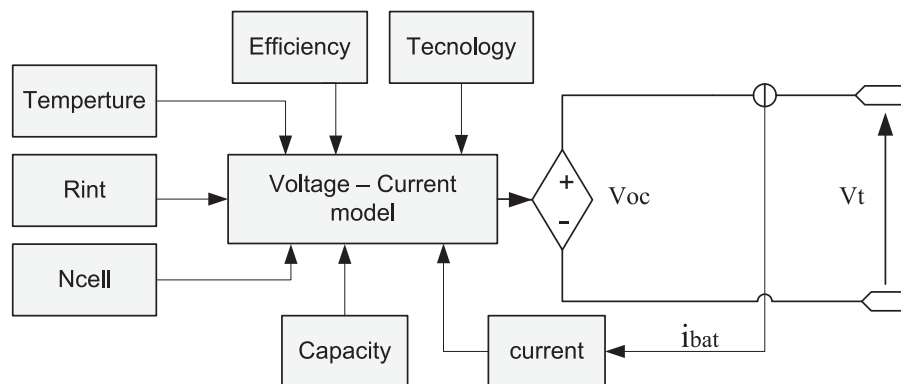


Fig. 20. Another generic battery model.

phenomenon between charge and discharge cycles [42]. Eqs. (11) and (12) can be revised by using state of charge. Eq. (13) shows that when the state of charge decreases, the voltage drops, and polarization overvoltage impact increases in the discharge cycle. In addition, with regard to (13), the polarization overvoltage impact is negligible in the proximity of the full battery capacity but becomes a predominant part as the state of charge collapses:

$$V_{\text{dis}} = E_0 - K_{\text{dr}} \frac{1}{\text{SOC}} i^* - R_0 i - K_{\text{dv}} \left(\frac{1}{\text{SOC}} - 1 \right) + \text{Exp}(t) \quad (13)$$

Capacity of the battery does not vary with the current. The temperature effect is neglected in this model. Also, battery aging has not been considered. The self-discharge is not entered. These factors can be obtained in a more complete mathematical model of the battery shown in Fig. 19. The battery parameters vary during the lifetime of the battery to supply an ageing profile and many other agents affect battery performance [42]. Parameters required for the mathematical modeling of the battery can be obtained based on the characteristics of the battery manufacturer. One approach is to build a parameter derive system which is established upon equations extracted from critical points of the characteristics in steady state. Afterwards, the model parameters can be achieved resolving the system equations. Another way is getting model parameters through regression method. Another generic model is shown in Fig. 20. The model consists of several blocks representing various sectors of the battery. Each block has various equations for each technology. The suitable equations are chosen based on a specific technology. The internal resistance of the cell, ambient temperature, number of cells, capacity, efficiency and other similar indices are represented by the input blocks. This model can be implemented in any simulations [43].

These models have been applied to an electric/hybrid vehicle modeling and simulation.

8. Conclusion

In this paper, electrical circuit modeling of batteries was classified into six main types of models consisting of (a) simple models, (b) Thevenin-based models, (c) impedance-based models, (d) runtime-based circuit models, (e) combined electrical circuit-based models, and (f) generic-based models. The electrical circuit models are implemented in dynamic simulation studies such as wind energy conversion systems, photovoltaic systems, and electric/hybrid vehicles systems. The Thevenin models have a good transient response in a significant SOC and in a constant V_{oc} ; however DC response and the battery runtime predictions are not adequately carried out. Although some components have been augmented to the models in order to improve these defects (such as utilization of a variable capacitor), the runtime error, voltage error and complication increase. The effects of temperature and SOC variations have not been generally considered in this model. They are suitable for transient studies but AC response is limited. Impedance-based model uses electrochemical impedance spectroscopy and complex impedance Z_{ac} to fit the impedance spectra. The fitting mechanisms have a difficult and complicated process. The ambient temperature and SOC variations have been ignored in this model too. The AC response has been modeled well but transient response is limited. The DC response and battery runtime prediction have not been considered. The runtime-based model is utilized to simulate the DC voltage response and runtime of a battery in a constant discharge current. This model is complex. It is

not suitable for the prediction of DC voltage response and runtime when the discharge current changes. Thus, it is not accurate as a model in AC response and its transient response is limited. Combined-based model consists of a blend of Thevenin, impedance, and runtime-based models. It is capable to predict the DC voltage response, runtime and transient response simultaneously. This model is more accurate and more comprehensive than other models. Finally, a generic battery model is an accurate and general model implemented in the modeling of different battery technologies. This model has been included in Simulink demo (Simpower system) as a part of hybrid/electric vehicles simulations.

References

- [1] Bashash S, Moura SJ, Forman JC, Fathy HK. Plug-in hybrid electric vehicle charge pattern optimization for energy cost and battery longevity. *J Power Sources* 2011;196(1):541–9.
- [2] Zandi M, Payman A, Martin JP, Pierfederici S, Davat B, Meibody-Tabar F. Energy management of a fuel cell/super capacitor/battery power source for electric vehicular applications. *IEEE Trans Veh Technol* 2011;60(2):433–43.
- [3] Musavi F, Eberle W, Dunford WG. A high-performance single-phase AC–DC power factor corrected boost converter for plug in hybrid electric vehicle battery chargers. *IEEE Energy Convers Cong Expo* 2010:3588–95.
- [4] Lukic SM, Cao J, Bansal RC, Rodriguez F, Emadi A. Energy storage systems for automotive applications. *IEEE Trans Ind Electron* 2008;55(6 (June)):2258–67.
- [5] Dallinger David, Wietschel Martin. Grid integration of intermittent renewable energy sources using price-responsive plug-in electric vehicles. *Renew Sustain Energy Rev* 2012;16(5):3370–82.
- [6] Tie Siang Fui, Tan Chee Wei. A review of energy sources and energy management system in electric vehicles. *Renew Sustain Energy Rev* 2013;20:82–102.
- [7] Richardson David B. Electric vehicles and the electric grid: a review of modeling approaches, impacts, and renewable energy integration. *Renew Sustain Energy Rev* 2013;19:247–54.
- [8] Mousavi SM, An G. Autonomous hybrid energy system of wind/tidal/micro-turbine/battery storage. *Int J Electr Power Energy Syst* 2012;43(1):1144–54.
- [9] Kalantar M, Mousavi G. SM. Dynamic behavior of a stand-alone hybrid power generation system of wind turbine, microturbine, solar array and battery storage. *Appl Energy* 2010;87(10 (October)):3051–64.
- [10] Hasan Nor Shahida, Hassan Mohammad Yusri, Majid Md Shah, Rahman Hasimah Abdul. Review of storage schemes for wind energy systems. *Renew Sustain Energy Rev* 2013;21 (May):237–47.
- [11] Toledo Olga Moraes, Filho Delly Oliveira, Alves Cardoso Diniz Antônia Sônia. Distributed photovoltaic generation and energy storage systems: a review. *Renew Sustain Energy Rev* 2010;14 (May):506–11.
- [12] Díaz-González Francisco, Sumper Andreas, Gomis-Bellmunt Oriol, Villafañila-Robles Roberto. A review of energy storage technologies for wind power applications. *Renew Sustain Energy Rev* 2012;16 (May):2154–71.
- [13] Zhou Zhibin, Benbouzid Mohamed, Charpentier Jean Frédéric, Scuiller Franck, Tang Tianhao. A review of energy storage technologies for marine current energy systems. *Renew Sustain Energy Rev* 2013;18 (May):390–400.
- [14] Hill CA. Satellite battery technology: a tutorial overview. *IEEE Aerosp Electron Syst Mag* 2011;26(6 (June)):38–43.
- [15] Yu Zhang, Zhenhua Jiang, Xunwei Yu. Control strategies for battery/ super-capacitor hybrid energy storage system. *IEEE Conf. on energy* 2008:1–6.
- [16] Duugal RA. Power and life extension of battery ultra-capacitor hybrids. *IEEE Trans Compon Packag Technol* 2002;25(1):120–31.
- [17] Zhan CJ, Wu XG, Kromlidis S, Ramachandaramurthy VK, Burnes M, Jenkins N, Ruddell AJ. Two electrical models of lead acid battery used in dynamic voltage resistor. *IEE pro. Gene. Transm. Distrib* 2003;150(2 (March)):175–82.
- [18] Chan HJ, Sutanto D. Lead acid storage batteries for uninterruptable power supply (UPS) application. In: *International telecommunication energy conference*; 1979. p. 226–30.
- [19] Kim YH, Ha HD. Design of interface circuits with electrical battery models. *IEEE Trans Ind Electron* 1997;44(1):81–6.
- [20] Ceraolo Massimo. New dynamic models of lead acid batteries. *IEEE Trans Power Syst* 2000;15(4):1184–90.
- [21] Valenciaga F, Puleston PF, Battaiotto PE, Mantz RJ. passivity sliding mode control of a standalone hybrid generation system. *IEE proc. Control theory appl.* 2000;147(6):680–6.
- [22] Mathias Dur, Andrew Cruden, Gair Sinclair, McDonald JR. Dynamic model of a lead-acid battery for use in a domestic fuel cell system. *J Power Sources* 2006;161(2 (October)):1400–11.
- [23] Jean Paul Cun, Fiorina JN, Fraisse M, Mabboux H. The Experience of a UPS Company in Advanced Battery Monitoring. *IEEE conf., 18th international telecommunication energy*, 1996, pp. 646–53.
- [24] Kim YH, Ha HD. Design of interface circuits with electrical battery models. *IEEE Trans Ind Electron* 1997;44(1):81–6.
- [25] Chan H, Sutanto D. A new battery model for used with battery energy storage system and electric vehicle power system. *IEEE Power Eng Soc* 2000:470–5.
- [26] Marcos J, Laga A, Penalver Cm, Doval J, Nogueira A, Castro C, et al., An approach to real behavior modeling for traction lead acid batteries. In: *IEEE 32nd annual power electronics specialists conference*, vol. 2; 2001. p. 620–24.
- [27] Daowd M, Omar N, Verbrugge B, Bossche PVD, Mierlo JV. Battery models parameters estimation based on Matlab/ Simulink, the 25 th world bat., hybrid and FC elec. Veh. Symp. & exh., Nov. 2010.
- [28] Williamson J, Rimmalapudi S, Emadi A. C. Electrical modeling of renewable energy sources and energy storage devices. *J Power Electron* 2004;4(2 (April)).
- [29] Appelbaum J, Weiss R. An electrical model of the lead acid battery. In: *IEEE conference on telecommunication energy*; October 1982. p. 304–07.
- [30] Salameh ZM, Casacca MA, Lynch WA. A mathematical model for leadacid batteries. *IEEE Trans Energy Convers* 1992;7(1 (March)):93–8.
- [31] Masoum MA, Badejani SMM, Fuchs EF. Microprocessor controlled new class of optimal battery charger for photovoltaic applications. *IEEE Trans. On energy conversion* 2004;19(3):599–606.
- [32] Shuo Pang, Jay Farrell, Jie Du, Matthew Barth. Battery state-of charge estimation. In: *Proceedings of the American control conference*, vol. 2; June 2001. p. 1644.1649.
- [33] Chiasson J, Vairamohan B. Estimating the state of charge of a battery. *IEEE Trans Control Syst Technol* 2005;13(3):465–70.
- [34] Kuhn E, Forgez C, Friedrich G. Modeling diffusive phenomena using non integerderivatives. *Eur Phys J Appl Phys* 2004;25(3):183–90.
- [35] Suresh P, Shukla AK, Munichandraiah N. Temperature dependence studies of a.c. impedance of lithium-ion cells. *J Appl Electrochem* 2002;32(3):267–73.
- [36] Zhang Y, Wang CY. Cycle-life characterization of automotive lithium-ion batteries with LiNiO₂ cathode. *J Electrochem Soc* 2009;156(7):A527–35.
- [37] Chen LR. A design of an optimal battery pulse system by frequency varied technique. *IEEE Trans Ind Electr* 2007;54(1):398–405.
- [38] Buller S, Thele M, Doncker RWD, Karden E. Impedance based simulation models of supercapacitors and Li-ion batteries for power electronic applications. *IEEE Trans Ind Appl* 2005;41(3 (May–June)):742–7.
- [39] Chen M, Rincón-Mora GA. Accurate electrical battery model capable of predicting runtime and IV performance. *IEEE Trans Energy Convers* 2006;21(2):504–11.
- [40] Zhang H, Mo-Yuen Chow. Comprehensive dynamic battery modeling for PHEV applications. In: *Proceedings of 2010 IEEE PES general meeting*, Minneapolis, MN; July 26–29, 2010.
- [41] Tremblay O, Dessaint LA, Dekkiche AI. A generic battery model for the dynamic simulation of hybrid electric vehicles. In: *Proceedings of 2007 IEEE vehicle power and propulsion conference*, Arlington, TX; September 9–12, 2007. p. 284–9.
- [42] Tremblay O, Dessaint LA. Experimental validation of a battery dynamic model for EV applications. *World Electr Veh J* 2032-6653 2009;3.
- [43] Prieto R, Oliver JA, Reglero I, Cobos JA. Generic battery model based on a parametric implementation. In: *IEEE applied power electronics conference*; September 2009.
- [44] Hannan MA, Azidin FA, Mohamed A. Hybrid electric vehicles and their challenges: A review. *renewable and sustainable energy reviews* 2014;29:135–50.